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## Thermodynamics of the Mg–B system: Implications for the deposition of MgB<sub>2</sub> thin films

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We have studied the thermodynamics of the Mg-B system with the calculation of phase diagrams modeling technique using a computerized optimization procedure. Temperature-composition, pressure-composition, and pressure-temperature phase diagrams under different conditions are obtained. The results provide helpful insights into appropriate processing conditions for thin films of the superconducting phase, MgB<sub>2</sub>, including the identification of the pressure-temperature region for adsorption-controlled growth. Due to the high volatility of Mg, MgB<sub>2</sub> is thermodynamically stable only under fairly high-Mg overpressures for likely growth temperatures. This places severe temperature constraints on deposition techniques employing high-vacuum conditions. © 2001 American Institute of Physics. [DOI: 10.1063/1.1376145]

The recent discovery of superconductivity in  $MgB_2$  at 39 K has generated great interest.<sup>1,2</sup> MgB<sub>2</sub> has the highest  $T_c$ known for nonoxide compounds and appears to become superconducting by the BCS mechanism.<sup>3</sup> Its coherence length is longer than those in high-temperature cuprate superconductors, and its grain boundaries have a far less detrimental effect on superconducting current transport.<sup>4</sup> These properties hold tremendous promise for various large-scale and electronic applications. However, due to the high volatility of Mg, difficulties in fabricating MgB<sub>2</sub> thin films by in situ deposition are anticipated. On the other hand, such volatility can greatly simplify composition control by enabling adsorption-controlled film growth<sup>5</sup> as is extensively used for the growth of III-V and II-VI compound semiconductors. It has been demonstrated for numerous materials containing a volatile constituent that an understanding of the thermodynamics of the system can help identify the appropriate growth region for these materials.<sup>6-10</sup>

Although MgB<sub>2</sub> has been known and structurally characterized since the mid-1950s,<sup>11</sup> no detailed thermodynamics information is available in the literature.<sup>12</sup> In this letter, we present a thermodynamic analysis of the Mg-B system with the thermodynamic calculation of phase diagrams (CALPHAD) modeling technique using a computerized optimization procedure. We have obtained temperaturepressurecomposition, pressure-composition, and temperature phase diagrams under various conditions. We find that the MgB<sub>2</sub> phase is thermodynamically stable only under high-Mg partial pressures. This condition favors deposition techniques that can maintain a high flux of Mg, which may operate in a pressure-temperature window and exploit the automatic composition control benefit that accompanies adsorption-controlled growth.

In the CALPHAD approach, the Gibbs energies of indi-

vidual phases in a system are constructed with models primarily based on the crystal structures of the phases.<sup>13</sup> For pure elements, the most commonly used model is suggested by the Scientific Group Thermodata Europe (SGTE) and the SGTE data have been compiled by Dinsdale.<sup>14</sup> By combining thermodynamic descriptions of unary systems with binary experimental data, thermodynamic descriptions of binary systems are then developed. In the Mg-B system, there are three intermediate compounds, MgB<sub>2</sub>, MgB<sub>4</sub>, and MgB<sub>7</sub>, in addition to the gas, liquid, and solid (hcp) magnesium phases and the  $\beta$ -rhombohedral boron solid phase.<sup>15</sup> The Gibbs energy for the intermediate compounds is written using the two-sublattice model as

$$G_m^{\text{MgB}_b} = {}^0G_{\text{Mg}}^{\text{solid}} + b^0G_{\text{B}}^{\text{solid}} + \Delta G_f^{\text{MgB}_b},\tag{1}$$

where *b* is 2, 4, or 7 for the three intermediate phases, respectively,  ${}^{0}G_{Mg}^{\text{solid}}$  and  ${}^{0}G_{B}^{\text{solid}}$  are Gibbs energies for Mg and B solids, respectively, and  $\Delta G_{f}^{\text{MgB}_{b}}$  is the Gibbs energy of formation for  $MgB_h$ . Using the experimentally measured enthalpy of formation and estimated decomposition temperatures,  $\Delta G_f^{\text{MgB}_b}$  is evaluated with the Thermo–Calc program<sup>16</sup> for MgB<sub>2</sub>, MgB<sub>4</sub>, and MgB<sub>7</sub>, and the phase equilibria are then calculated.

In Fig. 1, the calculated temperature-composition phase diagrams for the Mg-B system at (a) 1 atm, (b) 1 Torr, and (c) 1 mTorr are plotted. The labels "Solid," "Liquid," and "Gas" represent the Mg-rich solid, liquid, and gas phases, respectively. The result of our calculation for 1 atm pressure is consistent with the published Mg-B phase diagram,<sup>12</sup> which confirms the powerful capability of the CALPHAD technique. Below 1545 °C and for the atomic Mg:B ratio,  $x_{Mg}/x_{B}$ , greater than 1:2, the MgB<sub>2</sub> phase coexists with the Mg-rich solid, liquid, and gas phases at various temperatures. Above 1545 °C MgB<sub>2</sub> decomposes into a mixture of MgB<sub>4</sub> and Mg vapor. If  $1:4 < x_{Mg}/x_B < 1:2$  and the temperature is below 1545 °C, MgB<sub>2</sub> coexists with MgB<sub>4</sub>. When the pres-

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FIG. 1. Temperature–composition phase diagrams of the Mg–B system under the pressures of (a) 1 atm, (b) 1 Torr, and (c) 1 mTorr.

sure is reduced to 1 Torr, the phase diagram changes dramatically. Since the pressure is lower than the triple-point pressure of Mg (650 °C 2.93 Torr), the liquid phase of Mg completely disappears. The decomposition temperature of MgB<sub>2</sub> decreases to 912 °C. This temperature decreases further to 603 °C at the pressure of 1 mTorr. Evidently, the pressure has significant influence on the decomposition temperature of MgB<sub>2</sub>, which can be very low, thus severely limiting the thin-film deposition temperature.

The kinetics of crystal growth require that an *in-situ* film deposition process takes place at sufficiently high temperatures. The optimum temperature for expitaxial growth is typically about one half of the melting temperature,  $T_m$  (in Kelvin), although the minimum temperature can be much lower.<sup>17</sup> For example, the minimum epitaxial growth temperature for metals is about  $T_m/8$ .<sup>18</sup> Thermodynamic calculation shows that MgB<sub>2</sub> melts congruently at 2430 °C (~2700 K) with pressure higher than 49 000 Torr, therefore, the optimum temperature for deposition of epitaxial MgB<sub>2</sub> films is around ~1080 °C (1350 K). For MgB<sub>2</sub> to be stable at 1080 °C, a Mg partial pressure of at least 11 Torr is required, which is impossible for many thin film deposition deposition.



FIG. 2. Pressure-composition phase diagram of the Mg–B system at 850  $^{\circ}\mathrm{C}.$ 

niques. This encourages film growth at temperatures lower than optimal but nonetheless sufficient for epitaxial growth. In Fig. 2, the pressure–composition phase diagram at 850 °C is shown. At this temperature,  $MgB_2$  is thermodynamically stable only above a Mg partial pressure of 340 mTorr. Below this pressure  $MgB_2$  will decompose and only Mg vapor,  $MgB_4$ ,  $MgB_7$ , or solid B can be obtained.

Figures 1 and 2 illustrate the automatic composition control benefit that accompanies the adsorption-controlled growth. From a thermodynamic perspective, deposition of a single-phase MgB<sub>2</sub> film becomes easy when the growth conditions (substrate temperature and Mg overpressure) fall within a window where the thermodynamically-stable phases are the desired MgB<sub>2</sub> phase and gas phases. Within this growth window MgB<sub>2</sub> does not decompose and excess Mg does not condense on the MgB<sub>2</sub> surface, thus the formation of single-phase MgB<sub>2</sub> is adsorption-controlled and automatic. From the figures we find that this composition window, marked as ''Gas+MgB<sub>2</sub>,'' is large. As long as the Mg:B ratio is above the stoichiometric 1:2, any amount of extra Mg above the stoichiometry will be vaporized and the desired MgB<sub>2</sub> phase will result. The more critical requirement for controlling the stoichiometry is to avoid insufficient Mg supply, which will lead to MgB<sub>4</sub>, MgB<sub>7</sub>, or solid B phases.

The thermodynamic stability window for MgB<sub>2</sub> film deposition (the "Gas+MgB<sub>2</sub>" region) is best illustrated by the pressure-temperature phase diagram shown in Fig. 3. This phase diagram is essentially the same for all compositions with  $x_{Mg}/x_B \le 1:2$ . If the Mg overpressure is too low, it is thermodynamically favorable for MgB<sub>2</sub> to decompose into MgB<sub>4</sub> (+Gas). If it is too high, it is thermodynamically favorable for Mg to condense on to the MgB<sub>2</sub> surface. For a given deposition temperature, one can find the Mg partial pressure range to keep the MgB<sub>2</sub> phase thermodynamically stable. As seen in the figure, this range extends over about three orders of magnitude. The boundaries of the growth here to the terms of high-schedule persent boundaries. Boundaries to be approximately expressed by the following



FIG. 3. Pressure-temperature phase diagram for the Mg:B atomic ratio  $x_{Mg}/x_B \ge 1/2$ . The region of Gas+MgB<sub>2</sub> represents the thermodynamic stability window for the deposition of MgB<sub>2</sub> thin films.

equations:  $\log (P) = -7561/T + 8.673$  (the upper boundary with solid Mg), and  $\log (P) = -10142/T + 8.562$  (the lower boundary with MgB<sub>4</sub>), where *P* is in Torr and *T* in Kelvin.

The Mg partial pressure can be converted to Mg flux, *F*, from the deposition source using the formula  $F = P/\sqrt{2\pi mk_BT}$ , where *m* is the mass of Mg atom,<sup>19,20</sup> to determine the film deposition parameters. For example, at the optimum temperature of 1080 °C, the required Mg partial pressure of about 10 Torr is equivalent to an incident Mg flux of  $2 \times 10^{21}$  Mg atoms/(cm<sup>2</sup>s), or a Mg deposition rate of 0.5 mm/s if all the Mg atoms stick and form a Mg layer with bulk density. This is impossible for most thin film deposition techniques. One can sacrifice epitaxy for phase stability by lowering the growth temperature. For example, the highest tolerable Mg pressure for molecular beam epitaxy (MBE) is typically  $10^{-4}$  Torr.<sup>20</sup> From Fig. 3, this implies a maximum substrate temperature of about 534 °C (807 K) for MBE.

While the applicability of equilibrium thermodynamics to thin film growth has been established for many material systems, the non-equilibrium nature of specific deposition techniques can be quite important. For MgB<sub>2</sub>, a recent study has revealed a significant kinetic barrier to the thermal decomposition of MgB<sub>2</sub>.<sup>21</sup> This opens the possibility of using non-equilibrium routes to drive the formation reaction of MgB<sub>2</sub> to mitigate by as much as a factor of  $10^{-3}$  the high Mg pressures described in this letter.

In conclusion, the CALPHAD technique was used to develop a thermodynamic description of the Mg–B system. We find that MgB<sub>2</sub> is thermodynamically stable only under fairly high to very high Mg partial pressures at the temperature range appropriate for *in situ* epitaxial growth, implying that a large Mg flux must be delivered from the deposition source. This requirement favors deposition techniques that can maintain a large Mg flux over those where a large Mg flux is impractical. It should be pointed out that our approach considers only the equilibrium thermodynamic conditions, and the kinetics of the thin film growth could change the details of the phase stability window.

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